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④ A process for the manufacture of two-wheeled-vehicle tires and tires obtained thereby.

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EP 0 461 646 B1

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Description

The present invention is concerned with a process for the manufacture of motor-driven vehicle tires, in particular for two-wheeled vehicles and more particularly for motorcycles, and the tires made by the process.

These tires have a particular structure and shape so that they can withstand use conditions completely different from those in which normal tires for four-wheel vehicles are used; it is in fact sufficient to remember that when curvilinear paths have to be taken it is not the travel direction of the tire which is altered but the vehicle position, which is inclined sideways towards the road surface during a turn.

For the above reason two-wheeled-vehicle tires must be capable of running with camber angles of very high value, in the order of 50° or more, against a normal value of 3° to 4° in four-wheeled-vehicle tires, the camber angle being continuously and uniformly altered: consequently these tires have a cross section which is very rounded, that is provided with a strong convexity in the crown, unlike other tires in which the transverse profile of the tread is almost flat.

This strong convexity in the crown involves problems during the tire molding step bringing about drawbacks and deterioration of quality in use.

It is known that a tire of the above type comprises a carcass of toroidal form, a tread band disposed on the crown of said carcass and an annular reinforcement structure, also known as belt, fitted between the carcass and the tread band.

In particular, in carcasses of the radial type, that is those having reinforcement cords lying in planes containing the rotational axis of the tire, the belt preferably comprises one or more layers of cords made of an appropriate reinforcement material, at least resistant to tensile stress, disposed in mutual side by side relation and all parallel to one another and oriented in a substantially circumferential direction.

This annular reinforcement structure must be circumferentially inextensible and be submitted to a tensile preloading when the tire is deflated, so that it can perform all the required functions when the tire is in use.

It is also known that a process for the manufacture of such radial tires as disclosed e.g. in US-A-3 960 628, substantially comprises the steps of disposing the carcass in the form of a cylindrical sleeve on an appropriate manufacturing drum; giving said carcass a toroidal form on the selfsame drum or on a different manufacturing drum; applying an annular reinforcement structure and the tread band to the crown of the toroidal carcass thus shaped; putting the carcass thus arranged within a

vulcanization mold of the type commonly referred to as "centripetal" which, in register with the tread, is provided with a ring of sectors radially movable inwardly and outwardly; expanding the carcass for the purpose of putting said belt in a preloaded condition and simultaneously closing the mold by a centripetal radial displacement of the sectors, so that a raised pattern formed by said sectors may penetrate into the tread band while carrying out the molding thereof.

The expansion of the carcass within the mold is usually known as "pulling" and corresponds to an increase of about 1.5% in the circumferential size of the tire. This process, in tires of the type having a high transverse convexity to which the present invention refers, gives rise to some drawbacks which are particularly troublesome in tires in which the tread pattern has very deep hollows or grooves.

In fact, as previously stated, the belt must be an almost inextensible circumferential structure, which means that the maximum permissible pulling cannot exceed the above stated value corresponding to a similar percent increase in the diameter thereof.

If the maximum depth of the hollows in the tread pattern is higher than this value it is apparent that the overall pattern molding can only be achieved by making the ribs present on the mold sectors penetrate into the thickness of the tread band and therefore the deeper the rib penetration is, the greater the portion of hollow formed in this manner.

It is however to be noted that while the expansion of the carcass is substantially radial at any point, and therefore the hollow portions formed as a result of the movement of the tread band against the sector ribs have a certain radial height, on the contrary the movement of each sector against the tread band is radial only at its axis of symmetry, whereas all other points move in a direction parallel to said axis and therefore not at right angles to the profile of the tire carcass, thereby molding hollows that are offset and displaced with respect to the desired pattern.

The phenomenon is increasingly more serious at the sector ribs which are more spaced apart from the axis of symmetry and for tires having a stronger convexity, particularly in the transverse direction.

In order to solve this problem the expansibility of the belt should be increased so as to increase the depth percent of the hollow formed by the movement of the tread band against the mold sectors (at the most as far as the value of 100%), but this would require a belt having a very expandable circumference which is contrary to the requirements of the tire in use.

The manufacture of a belt which is extensible only during the molding step by the use of the presently adopted cords made of high-resistant materials such as Kevlar (registered trademark available from Du Pont) or steel, but laid down loosely, that is in an undulated manner, or in compression, is not feasible due to the difficulties arising in connection with the process; actually the number of problems created by such a working process is greater than that of the problems thus solved.

Neither does the use of very extensible and heat-shrinkable textile materials such as nylon enable the problem to be solved, since these materials are unable to withstand stresses arising during the use of the tire without undergoing important deformations, in particular due to the effects of centrifugal force connected with high speed of the vehicle, which can even reach values in the order of 300 kilometers per hour.

The applicant has now devised a new process for the manufacture of tires of the type discussed above, and in particular a process for carcass shaping and belt manufacture enabling all the above problems to be solved and still other problems that will be disclosed hereinafter, so that the object of the present invention is a process for the manufacture of tires for motor-cycles capable of offering high performances, and the tires thus obtained that are in particular free from structural and molding faults that could adversely affect their behavior in use.

One aspect of the invention is to provide a process for the manufacture of tires for vehicle wheels comprising the following steps:

- manufacturing a tire carcass in the form of a cylindrical sleeve, by producing a tubular element of rubberized fabric reinforced with cords disposed substantially parallel to the axis of said sleeve and folding back the ends of the cords of said tubular element about one of a pair of annular metal bead cores which are circumferentially inextensible, said bead cores lying in planes perpendicular to the sleeve axis;
- shaping said tubular element into a torus by radially expanding the sleeve wall and moving said bead cores close to each other in an axial direction, so that a first toroidal configuration is formed;
- assembling a belt structure to the crown of said torically-shaped carcass, which belt structure comprises cords oriented in a substantially circumferential direction disposed in mutual side by side parallel relation, and superposing a tread band on said belt at a radially outer position thereof;

- 5 - introducing the assembled tire into a vulcanization mold;
- closing said mold and expanding the carcass against the mold surface, so that it reaches its final toroidal configuration, so as to achieve the molding of the tread pattern into the tread band in particular; and
- vulcanizing said carcass, the process being characterized by the fact of:
- 10 - making said belt using cords of a high-elongation type exhibiting, in their load-elongation diagram, a curvilinear portion mutually connecting two substantially rectilinear lengths to each other, which lengths are of different inclination relative to the axes of said diagram, and
- 15 - moving said annular bead cores coaxially away from each other during the toroidal shaping of said tubular element until a mutual axial distance is reached which corresponds to an intermediate toroidal configuration of smaller diameter than that of said first toroidal conformation, and exhibits a deviation of predetermined value from said final toroidal conformation, the value of the center axial distance between said annular bead cores being given by the load-elongation diagram of said belt cords, so that the expansion of said carcass in said mold to the final toroidal configuration, puts said belt cords in a tensile condition (preloading) corresponding to a point of said diagram located within said curvilinear portion.

Preferably said point will be located close to the end of said curvilinear portion corresponding to the highest elongation value.

In a very convenient manner, said cords are metal cords oriented in the same way and exhibiting an ultimate elongation included between 4% and 8% and which have been previously rubberized.

Conveniently said belt structure can be made by wrapping one or more turns of one or more strips of sufficient width around said carcass, which strips are formed with rubberized fabric reinforced with said high-elongation cords, overlapping the ends of said strip or strips over a portion in the order of 20 mm to 50 mm, or wrapping a single high-elongation cord continuously and repeatedly around said carcass going on in an axial direction from one end of the carcass to the other.

A different way for making said belt comprises helicoidally wrapping or coiling a tape of rubberized fabric of two or more (usually ten at the most) high-elongation cords on said carcass, proceeding in an axial direction from one end to the other along the toroidal profile of the carcass. In addition, should the above coiling techniques be used, the

helical wrapping can also be carried out by simultaneously proceeding from the middle towards both ends of the carcass, or the other way round.

In keeping with a further aspect of the invention, a tire for two-wheeled vehicles is provided which comprises a carcass of toroidal form having a strong transverse convexity, having a crown portion and two sidewalls terminating in beads for anchoring to a corresponding mounting rim, a tread band located on the crown of said carcass and having a convexity ratio in the range of 0.15 to 0.45, and a circumferentially inextensible belt structure interposed between said carcass and tread band, said annular reinforcement structure comprising a plurality of cord coils disposed in axial side by side relation, extending from one end of said structure to the other according to an angle almost of zero value relative to the circumferential direction of the tire, characterized in that said reinforcement cords are of the high-elongation type having a load-elongation diagram with a curvilinear portion connecting two substantially rectilinear lengths to each other, said lengths having a different inclination relative to the axes of said diagram, said cords in a vulcanized but not inflated and not loaded tire being in a tensile condition (preloading) corresponding to a point of said diagram located within said curvilinear portion and preferably in the vicinity of the end thereof corresponding to the greatest elongation value.

In a preferred embodiment, said reinforcement cords are metal cords oriented in the same way and having an ultimate elongation in the range of 4% to 8%.

The density of said cords in the above tire is preferable between 25 to 150 wires/dm and said cords can also be unevenly distributed in an axial direction, having concentrations and thinnings along said axial extension.

In addition, said high-elongation cords, if metallic, preferably consist of 1 to 4 strands, each strand in turn preferably consisting of 1 to 7 elementary wires, of a diameter in the range of 0.10 mm to 0.25 mm and the strands being helicoidally twisted together in the same way, their stranding pitch being between 10 mm. and 200 mm.

Advantageously the tire of the invention shows a substantially balanced and uniform behavior, characterized by the fact that the difference between the values of the drift thrust measured on the tire during rotation either clockwise or counterclockwise is less than 15% of the value of the maximum drift thrust.

The present invention will be best understood from the following detailed description and the accompanying drawings, given hereinafter by way of non-limiting example, in which: - Fig. 1 is an axial cross section of the tire of the invention;

- Fig. 2 is a qualitative and non-quantitative load-elongation diagram of the cords in accordance with the invention as compared with that of a cord type widely used in the present tires;

- Fig. 3 is a diagrammatic axial cross section showing the profile of toroidal conformation of a tire carcass in accordance with the invention in three different situations;

- Fig. 4 is a plan view of a portion of the belt structure of the tire shown in Fig. 1, in accordance with a specific embodiment.

Illustrating the tire of the invention first and referring particularly to Fig. 1, the tire comprises a carcass 1 formed with one or more rubberized fabric plies, having a toroidal conformation in right section in which the ends of the cords of the plies are folded back from the axial inside to the axial outside in a known manner around annular metal bead cores 3, provided, at an outer radial position, with a filler 2 of elastomeric material having appropriate rheometric features.

The crown of said carcass has a tread band 4 and an intermediate structure 5, usually known as a breaker or a belt, interposed between the tread band and the carcass.

The tire area comprising the bead core 3 and filler 2 constitutes the tire bead, for ensuring the anchoring of said tire to a corresponding mounting rim, not shown.

The area substantially included between the radially outer end of the filler 2 and the belt 5 end is referred to as a tire sidewall and constitutes the area of maximum flexibility, adapted to ensure comfort during the vehicle ride.

On the other hand, in some very particular embodiments the radial length of the sidewall area can be greatly reduced and in effect the sidewall can be eliminated when the radially outermost area of the filler 2 comes into contact with the radially inner end portion of the tread.

As can be seen from the tire shown in Fig. 1, though only examined from a qualitative point of view, motor-cycle tires have a very encircling tread, having a marked convexity in crown and, in effect, have a very rounded shoulder or could be considered not to have a shoulder between the sidewall and the tread band.

In particular this convexity is expressed by the value of the h/w ratio, where h represents the radial height of the tread relative to the reference line c-c passing through the radially inner ends of said tread, and w represents the maximum width of said tread, as shown in Fig. 1. For the tire of this invention the h/w value is preferably in the range of 0.15 to 0.45.

The exact defining of the tread ends, necessary for a reliable and objective definition of the

values of h and w , can be easily achieved due to the fact that the tread edge is in register with the maximum width of the tire and often ends in a sharp edge distinguishing the beginning of the sidewall and above all is adapted to enable the vehicle driver to appreciate when the maximum permissible camber angle is achieved, during a curvilinear ride path or on a curve in the road.

The radial height f of this edge or of the tread edge relative to a base line (b-b) of the beads, taken as reference line, conveniently although not necessarily is coincident with the ends of belt 5. The base line b-b connects the bead seating area of the two tire beads.

Formed in the thickness of the tread band is a raised pattern consisting of a plurality of hollows or grooves 4a, 4b, 4c and lands (not shown) obtained in a known manner by a molding operation carried out on the raw carcass in an appropriate mold.

The reasons for which in case of radial tires the mold must be of the type provided with radially movable sectors, the so-called centripetal type, have already been discussed.

For an appropriate behavior of the tire on the road, the direction of the grooves in relation to the thickness of the tread band must be substantially perpendicular to the tread surface at that point. It will be therefore recognized, and as can be seen from Fig. 1, that grooves of the same radial depth s actually have different developments into the tread, in a direction parallel to the equatorial plane m-m, depending upon the lying position of the groove in the tread, this development is equal to s for grooves located in the equatorial plane itself and proportionally decreases to a minimum value r for the grooves located at end (axial outer) positions.

On the contrary, when progressively moving axially from the middle towards the tread edges the width of said grooves in the axial direction increases.

It is therefore apparent, also from Fig. 1, that a correct molding of the axial outer end grooves of the tread cannot be achieved by a mold portion (sector) which is moved as a unit in a radial direction parallel to the line m-m, although provided with ribs that exactly correspond to the grooves 4b and 4c.

As regards the carcass, the reinforcement cords 11 (see Fig. 4) of the corresponding plies are of any convenient known material, even a metallic but preferably a textile material, and in this case more specifically of a material having a low modulus: among these materials the most appropriate for use are rayon, synthetic polyester fibers, and synthetic aliphatic poliamide fibers, generally known as nylon.

For example, in the illustrated embodiment the cords are made of rayon, that is a synthetic fiber

made from cellulose, extend axially from one bead to the other and are disposed at right angles to the circumferential direction of the tire, shown by the line m-m of the equatorial plane (center line), that is inclined to said line by an angle substantially equal to 90°.

Considering now the belt structure 5, it is formed with a plurality of cords 6 formed as coils disposed in axial side by side relation and extending from one axial end of the carcass crown portion to the other.

In a preferred embodiment of the invention said cords are metal cords oriented in the same way, of the high-elongation type, generally known as "HE cords", each consisting of a certain number, 1 to 5 and preferably 3 to 4, strands, each strand being comprised of a given number, 2 to 10 and preferably 4 to 7, of elementary wires having a diameter greater than 0.10 mm, preferably ranging between 0.12 and 0.25 mm. The strand wires and the cord strands are helically twisted together in the same way, according to the same twisting pitch or also according to different pitches for the wires and the strands (so called Lang's lay).

Obviously materials other than metal could also be used, provided that the cords have the same type of load-elongation diagram as above stated and mechanical strength features adapted to withstand the forces acting on the tire.

In particular the cord used in the prototype tire herein specifically described is a metal cord technically known as 3x7x0.12HE, that is a cord consisting of three strands, each of seven steel wires of 0.12 mm of diameter.

Due to the fact that the wire and strand twisting is carried out in the same way, the finished cord is coiled and substantially acquires the features of a spring and its particular load-elongation diagram shown in Fig. 2 by line HE depends on this fact.

In Fig. 2 there is a pair of reference axes perpendicular to each other with the load values C, that is the values of the tensile stresses applied to the cord, reproduced on the vertical axis, whereas on the horizontal axis the percent cord-elongation values L are reproduced. After submitting the cord to increasing tensile values, the corresponding elongations are measured and then marked in the plane defined by said pair of axes at points corresponding to each pair of applied load/achieved elongation values until the breaking point of the cord is reached.

One can immediately see that said diagram includes one substantially rectilinear length (OE) of weak sloping (strong elongations at low loads) followed by a still substantially rectilinear length (FZ) of strong sloping (small elongations at increasingly stronger loads), the two lengths being connected to each other by a curvilinear portion (EF) usually

referred to as a "knee".

By way of example, one can ascertain that the center line of said curvilinear portion EF corresponds to an elongation value ranging between about 1.5% and 3%; thus the explanation of the diagram can be easily understood.

The length of weak sloping corresponds to the elongation of the above described "spring"; in other words, during starting the elongation, first diagram portion, the helical coils of the cord extend, which brings about the wire straightening, as they exhibit a low tensile strength.

Going on in pulling, at the end of the knee the wires have already been completely extended, though twisted upon themselves and therefore they react to the applied pulling force by effect of the mechanical features of the material and no more by effect of the geometrical configuration of the cord. The material used is steel and consequently the cord elongation becomes moderate in spite of the increase in the applied force.

On the contrary, the cords normally used exhibit a load-elongation diagram as represented in Fig. 2 by line PA: in this case one can see the almost constant behavior of the cord submitted to pulling stresses, also characterized by a lower sloping than in the cord HE; the importance of this fact will be apparent in the following.

It will be now understood how the use of said cord has enabled the problem of the invention to be generally solved. The cord is in fact coiled on the carcass shaped according to an intermediate toroidal configuration, still far from the final toroidal configuration that it will take in the mold, under a rather weak tension in order not to deform the carcass structure.

In this manner the cord, with reference to its load-elongation diagram, is still in the vicinity of point O, in the starting length OE of weak sloping.

The belt is therefore substantially extensible at low values of the applied load, so that the following carcass expansion in the mold (obtained with load C1) can conveniently take high values in order to enable the molding of the tread band, and in particular of the pattern grooves through the complete depth thereof, by the displacement of the band against the projections of the sectors in the already closed mold, thereby ensuring a strictly radial molding at all points, whereas the belt cord or cords are brought to work to a point of the load-elongation diagram included in said curvilinear portion and preferably close to the outlet F from the knee and therefore already in a state of considerable tension (preloading) and in any case at the beginning of the length of maximum tensile strength.

The vulcanization of the tire makes this situation stable so that, during the use of the tire

5 (strong increase of the permanent load (C2-C1) by effect of the inflation pressure, and strong variable acting loads (C3-C2) by effect of speed) the belt works in the cord diagram portion external to point X.

10 It will be immediately noted that in this portion of the diagram the cords of the invention react with a lower elongation than the known cords, the load increase (C3-C2) being equal, that is the belt really behaves like a structure substantially inextensible in a circumferential direction, which ultimately brings about a better behavior of the tire of the invention, above all at high and very high speeds, as compared with the behavior of traditional tires.

15 Knowing this general behavior, it is possible to examine the process of the invention in more detail.

20 It is known that the process for the manufacture of tires usually provides the following already mentioned and well-known steps:

- 25 - manufacturing the tire carcass in the form of a cylindrical sleeve, by producing a tubular element of rubberized fabric reinforced with cords disposed substantially parallel to the axis of said sleeve and folding back the ends of the cords of said tubular element each about at least an annular metal bead core which is circumferentially inextensible, said bead cores lying in planes perpendicular to the sleeve axis;
- 30 - toroidally shaping said tubular element by radially expanding the sleeve wall centrally of the two bead cores and moving the bead cores close to each other in an axial direction, so that a first toroidal configuration is achieved;
- 35 - assembling a belt structure to said toroidally-shaped carcass, which belt structure comprises coils of cords oriented in a substantially circumferential direction and disposed in side by side relation, and a tread band on said belt at a radially outer position thereof;
- 40 - introducing the full carcass into a vulcanization mold of the centripetal type;
- 45 - closing said mold and expanding the carcass against the mold surface, so as to achieve the molding of the tread band in particular, and finally vulcanizing said carcass by an appropriate heat treatment to high temperature and pressure.

50 In accordance with the invention the above process is modified so as to accomplish a new process characterized by the fact of:

- 55 - making said belt using cords of the high-elongation type exhibiting, in their load-elongation diagram, (see Fig. 2) a curvilinear portion mutually connecting two substantially rectilinear lengths of different sloping, and

- moving said annular bead cores coaxially in relation to each other during the toroidal shaping of said tubular element until a mutual axial distance between the cores is reached which corresponds to an intermediate toroidal configuration of smaller diameter than that of said first toroidal configuration and exhibits a deviation of predetermined value from said final toroidal conformation, the value of the center distance between said annular cores being given by the load-elongation diagram of said belt cords, so that the expansion of said carcass in said mold into the final toroidal configuration, puts said belt cords in a tensile condition (preloading) corresponding to a point of said diagram located within said curvilinear portion.

Shown schematically in Fig. 3 are three different profiles (7, 8, 9) of toroidal conformation of the selfsame carcass, profile 7 representing the final conformation profile of the carcass plies in the vulcanization mold after the molding has taken place and during the vulcanization cycle. On all of the three profiles points A and B indicate the ends of the crown portion on which the belt structure is placed. It is obvious that the profiles must have the same linear extension from one bead to the other.

Profile 8 represents the first toroidal conformation profile of the carcass, before applying the belt in accordance with the known art; the difference $D-d_1$ corresponds to the usual expansion at the equatorial plane undergone by the carcass and the belt during the pulling step which, as seen, is equal to about 1.5%.

Profile 9 on the contrary represents the toroidal intermediate conformation profile of the selfsame carcass according to the process of the invention, that is that of the carcass ready to be assembled to the belt formed with high-elongation cords.

The diameter of profile 9 has a value d_2 lower than d_1 so that the increase $D-d_2$ corresponding to the expansion of the carcass during the pulling step corresponds to the elongation undergone by the belt cords.

Said intermediate toroidal conformation profile 9 of the carcass can be adjusted so that it may have a lower diameter than the profile 8 by stopping the axial movement of the beads close to each other at a convenient value c that is greater than b .

In this manner the expansion of the carcass as far as the profile 7 is achieved, is permitted by the fact that the mutual distance between the beads, commonly known as "posting" simultaneously passes from value c to the lower value a ; in this manner it is in fact possible to achieve an increase in the carcass diameter simultaneously with a constant linear extension of the toroidal profile of the

carcass itself.

Ideally the difference $D-d_2$ must correspond to the maximum depth s of the grooves in the tread pattern.

- 5 The elongation undergone by the belt cord or cords must be suitable to put said cords to a general point G (see Fig. 2) within the portion EF and preferably even to point F of the load-elongation diagram; in other words, G can vary at the inside of the knee but it will be preferably moved as much as possible towards the knee outlet or even to the boundary thereof, that is at the beginning of the greatly sloping portion.
- 10

- 15 The importance of the characteristic proper to the process for the manufacture of tires in accordance with the invention is now readily apparent and it consists in fixing the diameter of the toroidal conformation profile of the carcass depending upon the desired pulling value (in turn depending on the depth of the grooves in the tread pattern and/or the starting elongation of the cords used for the belt structure) and to control said diameter value by the selection of a corresponding value c for the bead posting.
- 20

- 25 The correlation between the pulling amount and the groove depth is well apparent; on the contrary as regards the high elongation cords it is to be noted that the starting capability of elongation of said cords (first diagram length) depends on many factors, among which the stranding pitch of the wires and strands, so that different cords have different capability of starting elongation. Which means that, the desired condition for the cord at the end of the vulcanization step being fixed as that of point F and all other conditions being equal, the portion OF will exhibit a variable length depending on the variation of the cord features.
- 30
- 35

- 40 In other words, different starting elongations (OL) must be allocated to the different types of cords so that they may reach the fixed condition of point F and therefore also the pulling to be given to the carcass before its vulcanization must be of different amount.

- 45 It is to be noted that this pulling does not necessarily need to be given within the mold but part of it could be given on the conformation drum after the belt has been assembled to the carcass.

- 50 It is instead important that the degree of pulling given within the mold should not be lower than the maximum depth of the grooves in the tread pattern, which depth is also variable depending upon the type of tire and pattern.

- 55 It will be therefore clear how the use of said high-elongation cords in the belt enables the desired value to be given to the belt pulling whereas the manufacturing process in accordance with the invention enables the pulling to be given to the belt, to be adjusted in accordance with the precise

features of the cord really used.

The manufacturing process being now known in its fundamental aspects, different embodiments are possible for the manufacture of the belt structure on the toroidally conformed carcass, all of them falling within the scope of the present invention.

According to a preferred embodiment the belt is made by helically wrapping continuously and repeatedly around the circumference of the tire a single optionally rubberized cord into coils disposed in side by side relation, proceeding axially from one end to the other of the crown portion of said carcass.

The wrapping pitch can be greater than the cord diameter so as to suitably control the density of the coils in the belt structure.

In this manner the angle at which the coils lie will not be strictly circumferential with respect to the tire but the coils will be oriented according to the angles v (Fig. 4) different from 0° relative to the equatorial plane.

However the value of said angle will always be lower than 2° and within this range, for high values of v , it could be convenient to modify also the lying angle of the cords 11 of the carcass plies (relative to the fundamental value of 90°) so as to maintain the correct cross angle between the carcass cords and the belt cords.

Preferably the coil density thus determined will be in the range of 25 to 150 cords/dm.

Alternatively, instead of helically wrapping a continuous single cord, a narrow tape containing several cords but preferably no more than 5 cords, could be conveniently wrapped around the carcass; in this manner the distance between the tape cords remains constant so that a possible variation in the tape coiling pitch p will bring about an uneven distribution of the coils in the belt structure thereby causing areas with closer coils followed by areas with less dense coils.

Fig. 4 shows an example of this belt embodiment, obtained by helically wrapping in an axial direction a tape 10 of rubberized fabric provided with three HE cords 6 coiled according to a pitch corresponding to five times the diameter of said cords.

In all cases of helical laying of the belt cords (either single cord or tape), the coiling can be conveniently carried out also starting from the middle of the crown portion, at the equatorial plane, and going on simultaneously in an axial direction towards both ends of said crown portion, or the other way about.

Many advantages are achieved with the tire of the present invention.

First of all the fact that a pulling greater than the usual one can be given to the raw carcass

5 within the mold enables a perfect tire molding, in particular as far as the deepest grooves of the tread pattern are concerned, whereas this capability of greater expansion of the belt on the raw carcass is completely eliminated on the vulcanized tire and therefore does not create disadvantages as regards the tire behavior in use.

10 In addition to the foregoing, due to the fact that the tread molding no longer takes place by penetration of the projections present on the sectors into the tread band thickness, it is not compulsory to use molds of the centripetal type, and therefore simpler molds consisting of two halves can be used.

15 In addition, the capability of greater expansion of the raw carcass improves the quality level of the finished tire since it enables possible unevenness in the structure and size of the used semi-finished products to be compensated for, in particular as regards the tread band thickness: it is in fact known that when the molding mainly takes place by penetration of the projections disposed on the sectors into the tread band thickness even light deviations of the band thickness from the predetermined values give rise to important irregularities in the distribution of the elastomeric material and considerable deformations in the underlying belt and carcass structure.

20 The process of the invention, by distributing this unevenness over the whole circumferential and transverse extension of the carcass by effect of said capability of greater expansion, produces a levelling of the imperfections, a greater uniformity in the structure being recovered and therefore accomplishing an increase in the quality level of the finished tire.

25 As regards the belt, only the laying of the cord layer at 0° has been described, but obviously it is understood that other cord layers or strips can exist together with this layer, which layers may be inclined to the equatorial plane and/or disposed circumferentially, according to the known art.

30 The important advantages achieved with the tire of the invention, in particular as regards the structural evenness and regular distribution of the rotating masses, are confirmed by the fact that the difference between the drift thrust values measured in the two rotational directions of the tire, is lower than 15% of the maximum detected thrust value.

35 50 Claims

1. A process for the manufacture of tires for vehicle wheels comprising the following steps:
 - 55 - manufacturing a tire carcass (1) in the form of a cylindrical sleeve, by producing a tubular element of rubberized fabric reinforced with cords disposed substan-

tially parallel to the axis of said sleeve and folding back the ends of the cords of said tubular element each about at least an annular metal bead core (3) which is circumferentially inextensible, said bead cores lying in planes perpendicular to the sleeve axis;

- toroidally shaping said tubular element by radially expanding the sleeve wall and moving said bead cores close to each other in an axial direction, so that a first toroidal configuration is achieved;
- assembling a belt structure (5) to said toroidally-shaped carcass, which belt structure comprises coils of cords (6) oriented in a substantially circumferential direction and disposed in side by side relation' and
- superposing a tread band (4) on said belt (5) at a radially outer position thereof;
- introducing the thus assembled tire into a vulcanization mold;
- closing said mold and expanding the carcass radially outwardly against the mold surface, so that it reaches its final toroidal configuration, so as to achieve the molding of the tread band; and
- vulcanizing said carcass,

the process being characterized by:

- making said belt (5) of high-elongation cords (6), said cords having in their load-elongation diagram, a curvilinear portion (E-F) mutually connecting two substantially rectilinear lengths (O-E; F-Z) of different inclination relative to the axes of said diagram, and
- moving said annular bead cores coaxially away from each other during the toroidal shaping of said tubular element until a mutual axial distance C between the bead cores is reached which corresponds to an intermediate toroidal configuration d_2 of smaller diameter than that d_1 of said first toroidal configuration and has a deviation (D-d2) of predetermined value from said final toroidal conformation, the value of the axial distance c between said annular bead cores being proportional to the load-elongation diagram of said belt cords, so that the expansion of said carcass in said mold to the final toroidal configuration puts said belt cords in a tensile preloading condition corresponding to a point G of said load-elongation diagram located within said curvilinear portion.

2. A process according to claim 1, including forming said belt (5) by the use of rubberized metal cords oriented in the same manner and having an ultimate elongation of between 4% and 8%.
3. A process according to claim 1, in which said belt (5) is made by wrapping at least one strip of rubberized fabric reinforced with said high-elongation cords around said carcass, overlapping the ends of said strips over a portion not lower than 20 mm in length.
4. A process according to claim 1, in which said belt is made by wrapping a single high-elongation cord continuously and repeatedly around said carcass and extending in an axial direction from one axial end of said carcass to the other.
5. A process according to claim 1, in which said belt is made by helically wrapping a tape (10) of rubberized fabric comprising two to ten high-elongation cords around said carcass, proceeding in an axial direction from one end of the carcass to the other.
6. A process according to claim 4, in which the helically wrapping of said metal high-elongation cords so as to make said belt is carried out by simultaneously proceeding from the middle towards both axial ends of the carcass.
7. A process according to claim 5, in which the helically wrapping of said metal high-elongation cords so as to make said belt is carried out by simultaneously proceeding from the middle towards both axial ends of the carcass.
8. In a tire for two-wheeled vehicles comprising
 - a carcass (1) of toroidal form having a strong transverse convexity, having one crown portion and two sidewalls terminating in beads for anchoring to a corresponding mounting rim,
 - a tread band (4) located on said crown and having a convexity ratio in the range of 0.15 to 0.45, and an annular, circumferentially inextensible reinforcement structure (5) interposed between said carcass and tread band, said annular reinforcement structure comprising a plurality of cord coils (6) disposed in axial side-by-side relation and extending from one axial end of said structure to the other at an angle almost of zero value relative to the equatorial plane of the tire, the improvement comprising said rein-

forcement cords being of a high-elongation type having a load-elongation diagram with a curvilinear portion (E-F) connecting two substantially rectilinear lengths (O-E; F-Z) to each other, said lengths having a different sloping, said cords in a vulcanized but not inflated and not loaded tire being in a tensile preloading condition corresponding to a point G of said diagram located within said curvilinear portion. 5

9. A tire according to claim 8, in which said reinforcement cords are metal cords oriented in the same manner and having an ultimate elongation in the range of 4% to 8%. 15

10. A tire according to claim 8, in which said reinforcement cords are disposed at a density of between 25 to 150 cords/dm. 20

11. A tire according to claim 8, in which said reinforcement cords are axially distributed in said belt structure in an uneven manner. 25

12. A tire according to claim 8, in which the difference between the values of the drift thrust measured on a tire rotating in either of the two rotational directions, is lower than 15% of the maximum value of said drift thrusts. 30

13. A tire according to claim 9, in which said metal cords oriented in the same manner and of the high elongation type are formed with 1 to 4 strands, each strand in turn preferably comprising 1 to 7 elementary wires, of a diameter in the range of 0.1 to 0.50 mm. 35

Patentansprüche 40

1. Verfahren zur Herstellung von Reifen für Fahrzeuge, welches die folgenden Schritte aufweist:

- Herstellen einer Reifenkappe (1) in Form einer zylindrischen Hülse durch Produzieren eines rohrförmigen Elements aus einem gummierten Textil, das mit Corden verstärkt ist, die im wesentlichen parallel zu der Achse der Hülse angeordnet werden, und Zurückfalten eines der Enden der Corde des rohrförmigen Elements um wenigstens einen ringförmigen Wulstkerne (3) aus Metall, der in Umfangsrichtung nicht dehnbar ist, wobei die Wulstkerne in Ebenen senkrecht zu der Hülsenachse liegen, 45
- Formen des rohrförmigen Elements zu einem Toroid durch radiales Ausspreizen 50

der Hülsenwand und Bewegen der Wulstkerne nahe zueinander in einer axialen Richtung, so daß eine erste toroidförmige Gestalt erreicht wird, 55

- Montieren eines Gurtaufbaus (5) an der zu einem Toroid geformten Kapsel, wobei der Gurtaufbau Windungen von Corden (6) aufweist, die im wesentlichen in Umfangsrichtung ausgerichtet und in einer nebeneinander liegenden Beziehung angeordnet sind,
- Auflegen eines Laufflächenbandes (4) auf den Gurt (5) in einer radial äußeren Lage von ihm,
- Einbringen des so montierten Reifens in eine Vulkanisierform,
- Schließen der Form und Expandieren der Kapsel radial nach außen gegen die Formfläche, so daß sie ihre endgültige toroidförmige Gestalt erreicht und die Formgebung des Laufflächenbandes erzielt wird, und
- Vulkanisieren der Kapsel,

gekennzeichnet durch

- Herstellen des Gurtes (5) aus Corden (6) mit hoher Dehnung, die in ihrem Spannungs-Dehnungs-Diagramm einen gekrümmten Abschnitt (E-F) haben, der zwei im wesentlichen gerade Längsstücke (O-E; F-Z) von unterschiedlicher Neigung bezüglich der Achsen des Diagramms miteinander verbindet, und
- Bewegen der ringförmigen Wulstkerne koaxial voneinander weg während der Formung des rohrförmigen Elements zu einem Toroid bis ein gegenseitiger axialer Abstand C zwischen den Wulstkerne erreicht ist, der einer toroidförmigen Zwischengestalt d2 entspricht, die einen Durchmesser hat, der kleiner ist als der d1 der ersten toroidförmigen Gestalt, und die eine Abweichung (D-d2) von einem vorgegebenen Wert von der endgültigen toroidförmigen Gestalt hat, wobei der Wert des axialen Abstands c zwischen den ringförmigen Wulstkerne proportional zu dem Spannungs-Dehnungs-Diagramm der Corde des Gurtes ist, so daß die Expansion der Kapsel in der Form zu der endgültigen toroidförmigen Gestalt die Corde des Gurtes in einen Zugvorspannungszustand bringt, der einem Punkt G des Spannungs-Dehnungs-Diagramms entspricht, der sich in dem gekrümmten Abschnitt befindet.

2. Verfahren nach Anspruch 1, welches das Formen des Gurtes (5) durch Verwendung von

gummierten Metallcorden einschließt, die in der gleichen Weise ausgerichtet sind und eine Bruchdehnung zwischen 4 % und 8 % haben.

3. Verfahren nach Anspruch 1, bei welchem der Gurt (5) dadurch hergestellt wird, daß wenigstens ein Band aus einem gummierter Textil, das mit Corden hoher Dehnung verstärkt ist, um die Karkasse gelegt wird, wobei sich die Enden der Bänder über einem Abschnitt von nicht weniger als 20 mm Länge überlappen. 5

4. Verfahren nach Anspruch 1, bei welchem der Gurt dadurch hergestellt wird, daß ein einziger Cord mit hoher Dehnung kontinuierlich und wiederholt um die Karkasse gelegt wird und sich in einer Axialrichtung von einem axialen Ende der Karkasse aus zu dem anderen erstreckt. 10

5. Verfahren nach Anspruch 1, bei welchem der Gurt dadurch hergestellt wird, daß ein Band (10) aus gummiertem Textil, das zwei bis zehn Corde hoher Dehnung aufweist, in einer Axialrichtung von einem Ende der Karkasse zum anderen fortschreitend wendelförmig um die Karkasse gewickelt wird. 15

6. Verfahren nach Anspruch 4, bei welchem das schraubenförmige Wickeln der Metallcorde mit hoher Dehnung zur Herstellung des Gurtes durch simultanes Fortschreiten von der Mitte zu den beiden axialen Enden der Karkasse hin durchgeführt wird. 20

7. Verfahren nach Anspruch 5, bei welchem das schraubenförmige Wickeln der Metallcorde mit hoher Dehnung zur Herstellung des Gurtes durch gleichzeitiges Fortschreiten von der Mitte zu den beiden axialen Enden der Karkasse hin durchgeführt wird. 25

8. Reifen für zweirädrige Fahrzeuge,

- mit einer eine Toroidform mit starker Querkonvexität aufweisenden Karkasse (1), die einen Scheitelabschnitt und zwei Seitenwände hat, die in Wulsten zum Verankern an einer entsprechenden Einbaufuge enden,
- mit einem Laufflächenband (4), das sich auf dem Scheitel befindet und ein Konvektionsverhältnis im Bereich von 0,15 bis 0,45 und einen ringförmigen, in Umfangsrichtung nicht dehnbaren Verstärkungsaufbau (5) hat, der zwischen der Karkasse und dem Laufflächenband angeordnet ist, wobei der ringförmige Verstärkungsaufbau eine Vielzahl von Cordwindungen (6) aufweist, die in einer axialen nebeneinander liegenden Beziehung angeordnet sind und sich von einem axialen Ende des Aufbaus zu dem anderen unter einem Winkel mit dem Wert von nahezu null bezogen auf die Äquatorebene des Reifens erstrecken, wobei die Verbesserung darin besteht

- daß die Verstärkungscorde eine hohe Dehnung und ein Spannungs-Dehnungs-Diagramm mit einem gekrümmten Abschnitt (E-F) haben, der zwei im wesentlichen gerade Längenstücke (O-E; F-Z) miteinander verbindet,
- daß diese Längenstücke eine unterschiedliche Neigung haben und
- daß sich die Corde in einem vulkanisierten, jedoch nicht aufgeblasenen und nicht belasteten Reifen in einem Zugvorspannungszustand entsprechend einem Punkt G des Diagramms befinden, der in dem gekrümmten Abschnitt liegt.

9. Reifen nach Anspruch 8, bei welchem die Verstärkungscorde Metallcorde sind, die in der gleichen Weise ausgerichtet sind und eine Bruchdehnung im Bereich von 4 % bis 8 % haben. 30

10. Reifen nach Anspruch 8, bei welchem die Verstärkungscorde mit einer Dichte zwischen 25 bis 150 Corde/dm angeordnet sind. 35

11. Reifen nach Anspruch 8, bei welchem die Verstärkungscorde in dem Gurtaufbau in ungleichförmiger Weise axial verteilt sind. 40

12. Reifen nach Anspruch 8, bei welchem die Differenz zwischen den Werten der an einem in jede der beiden Drehrichtungen drehenden Reifen gemessene Auswanderungsdruck niedriger als 15 % des maximalen Werts der Auswanderungsdruck ist. 45

13. Reifen nach Anspruch 9, bei welchem die in der gleichen Weise ausgerichteten Metallcorde mit hoher Dehnung mit 1 bis 4 Strängen geformt sind, wobei jeder Strang seinerseits vorzugsweise 1 bis 7 Elementardrähte mit einem Durchmesser im Bereich von 0,1 bis 0,50 mm aufweist. 50

Revendications

55 1. Procédé de fabrication de pneumatiques pour roues de véhicule comprenant les étapes suivantes :

- fabrication d'une carcasse de pneumatique (1) en forme de manchon cylindrique, par production d'un élément tubulaire fait d'un tissu caoutchouté renforcé par des câblés disposés sensiblement parallèlement à l'axe dudit manchon et repliage des extrémités de chaque câblé dudit élément tubulaire autour d'au moins une tringle de talon (3) annulaire et en métal, qui n'est pas extensible dans le sens de la circonférence, lesdites tringles de talon étant dans des plans perpendiculaires à l'axe du manchon, 5
- transformation en tore dudit élément tubulaire par dilatation radiale de la paroi du manchon et déplacement desdites tringles de talon pour les rapprocher les unes des autres dans la direction axiale de façon à obtenir une première configuration toroïdale, 10
- assemblage d'une structure de ceinture (5) sur ladite carcasse de forme toroïdale, laquelle structure de ceinture comprend des nappes de câblés (6) orientées dans une direction sensiblement circonférentielle et disposées côte-à-côte, et 15
- superposition d'une bande de roulement (4) sur ladite ceinture (5) en une position radialement extérieure de celle-ci, 20
- introduction du pneumatique ainsi assemblé dans un moule de vulcanisation, 25
- fermeture dudit moule et dilatation radiale de la carcasse vers l'extérieur pour l'amener contre la surface du moule de sorte qu'elle atteigne sa configuration toroïdale finale, de manière à terminer le moulage de la bande de roulement, et 30
- vulcanisation de ladite carcasse, 35

l'édit procédé étant caractérisé par :

- la fabrication de ladite ceinture (5) à l'aide de câblés (6) à fort allongement, lesdits câblés présentant dans leur diagramme d'allongement en fonction de la charge une partie curviligne (E-F) qui relie entre elles deux parties sensiblement rectilignes (O-E; F-Z) ayant des inclinaisons différentes par rapport aux axes dudit diagramme, et 40
- le déplacement coaxial desdites tringles de talon annulaires pour les écarter les unes des autres pendant la mise sous forme toroïdale dudit élément tubulaire jusqu'à ce qu'une distance axiale c entre les tringles de talon soit atteinte, laquelle correspond à une configuration toroïdale intermédiaire de diamètre d_2 plus petit que le diamètre d_1 de ladite première 45

configuration toroïdale et présente un écart ($D-d_2$) de valeur prédéterminée par rapport à ladite configuration toroïdale finale, la valeur de la distance axiale c entre lesdites tringles de talon annulaires étant proportionnelle au diagramme d'allongement en fonction de la charge desdits câblés de la ceinture, de sorte que la dilatation de ladite carcasse dans ledit moule jusqu'à ladite configuration toroïdale finale place lesdits câblés de la ceinture dans une situation de pré-tension qui correspond à un point G dudit diagramme de l'allongement en fonction de la charge situé dans ladite partie curviligne.

2. Procédé selon la revendication 1, comprenant la formation de ladite ceinture (5) à l'aide de câblés métalliques enrobés de caoutchouc, orientés de la même manière et ayant un allongement ultime compris entre 4 et 8 %. 20
3. Procédé selon la revendication 1, dans lequel ladite ceinture (5) est faite par enroulement autour de ladite carcasse d'au moins une bande de tissu caoutchouté renforcée par lesdits câblés à fort allongement, avec chevauchement des extrémités desdites bandes sur une partie qui n'a pas une longueur inférieure à 20 mm. 25
4. Procédé selon la revendication 1, dans lequel ladite ceinture est faite par enroulement de façon continue et répétée autour de ladite carcasse d'un seul câblé à fort allongement, qui s'étend dans la direction axiale d'une extrémité axiale à l'autre de ladite carcasse. 30
5. Procédé selon la revendication 1, dans lequel ladite ceinture est faite par enroulement en hélice autour de ladite carcasse d'un ruban (10) de tissu caoutchouté comprenant de deux à dix câblés à fort allongement, en avançant dans la direction axiale d'une extrémité à l'autre de ladite carcasse. 35
6. Procédé selon la revendication 4, dans lequel l'enroulement en hélice desdits câblés métalliques à fort allongement pour réaliser ladite ceinture est effectué par avancement simultané du milieu vers les deux extrémités axiales de la carcasse. 40
7. Procédé selon la revendication 5, dans lequel l'enroulement en hélice desdits câblés métalliques à fort allongement pour réaliser ladite ceinture est effectué par avancement simultané 45

du milieu vers les deux extrémités axiales de la carcasse.

8. Pneumatique pour véhicule à deux roues, comprenant :

- une carcasse (1) de forme toroïdale, présentant une forte convexité transversale et comprenant une partie formant couronne et deux flancs qui se terminent par des talons à ancrer sur une jante correspondante,
- une bande de roulement (4) située sur ladite couronne et présentant un taux de convexité dans la fourchette de 0,15 à 0,45, et
- une structure de renfort (5), annulaire et non extensible dans le sens de la circonférence, interposée entre ladite carcasse et ladite bande de roulement, ladite structure annulaire de renfort comprenant une pluralité de nappes de câblés (6) disposées côte-à-côte dans la direction axiale et s'étendant d'une extrémité axiale à l'autre de ladite structure en faisant un angle presque nul par rapport au plan équatorial du pneumatique,
l'amélioration consistant en ce que lesdits câblés de renforcement sont du type à fort allongement en ayant un diagramme de l'allongement en fonction de la charge qui comprend une partie curviligne (E-F) reliant entre elles deux parties sensiblement rectilignes (O-E; F-Z) qui ont des pentes différentes, lesdits câblés dans un pneumatique vulcanisé mais non gonflé et non chargé étant dans une situation de pré-tension qui correspond à un point G dudit diagramme situé dans ladite partie curviligne.

9. Pneumatique selon la revendication 8, dans lequel lesdits câblés de renfort sont des câbles métalliques orientés de la même manière et ayant un allongement ultime dans la fourchette de 4 à 8%.

10. Pneumatique selon la revendication 8, dans lequel lesdits câblés de renfort sont disposés avec une densité comprise entre 25 et 150 câbles par dm.

11. Pneumatique selon la revendication 8, dans lequel lesdits câblés de renfort sont répartis axialement dans ladite structure de ceinture de façon irrégulière.

12. Pneumatique selon la revendication 8, dans lequel la différence entre les valeurs de la

force de chasse mesurées sur un pneumatique tournant dans l'un et l'autre sens de rotation est inférieure à 15% de la valeur maximale desdites forces de chasse.

5 13. Pneumatique selon la revendication 9, dans lequel lesdits câbles métalliques orientés de la même manière et du type à fort allongement sont faits de 1 à 4 torons, chaque toron 10 comprenant lui-même de préférence entre 1 et 7 fils élémentaires d'un diamètre compris entre 0,1 et 0,50 mm.

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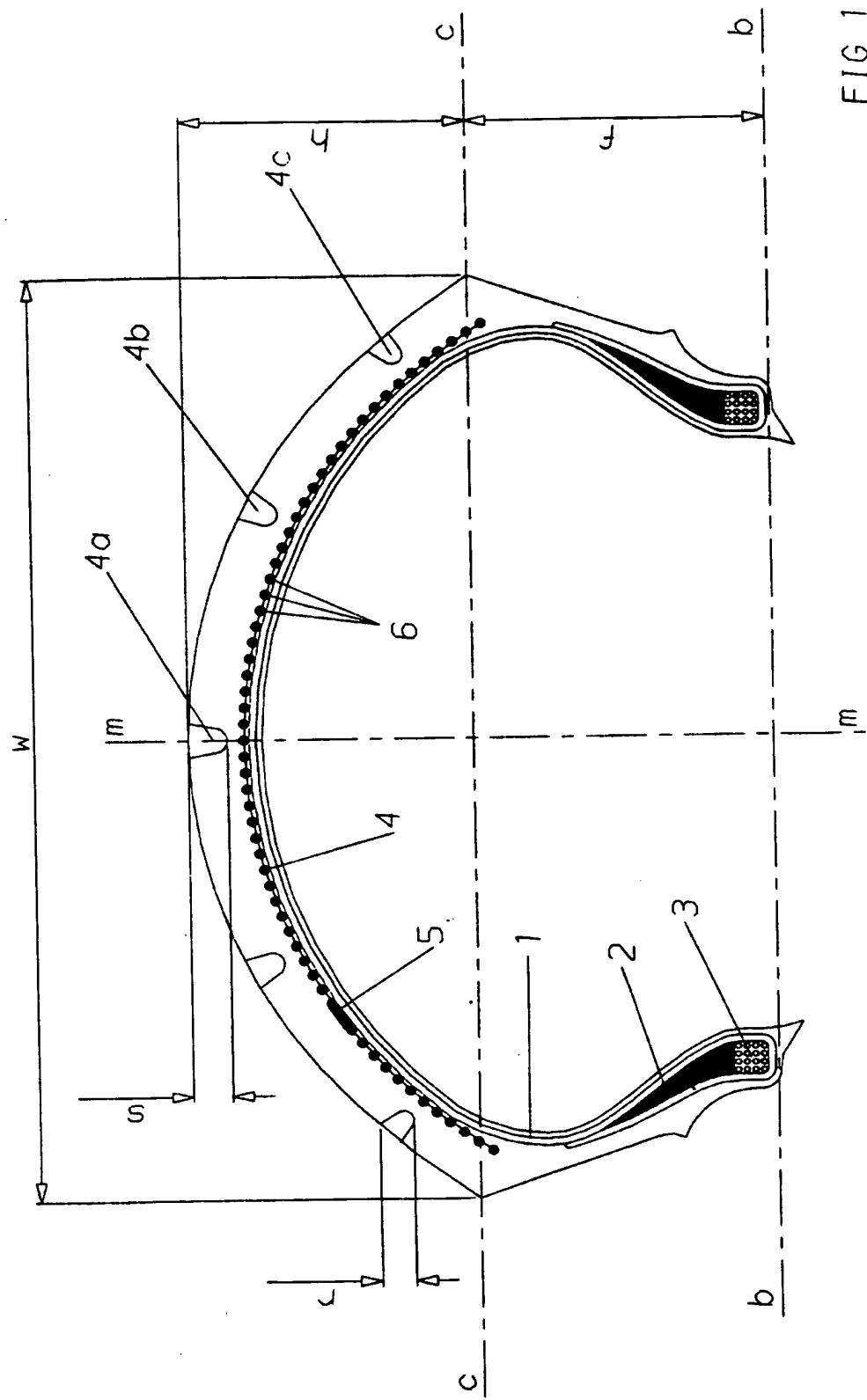
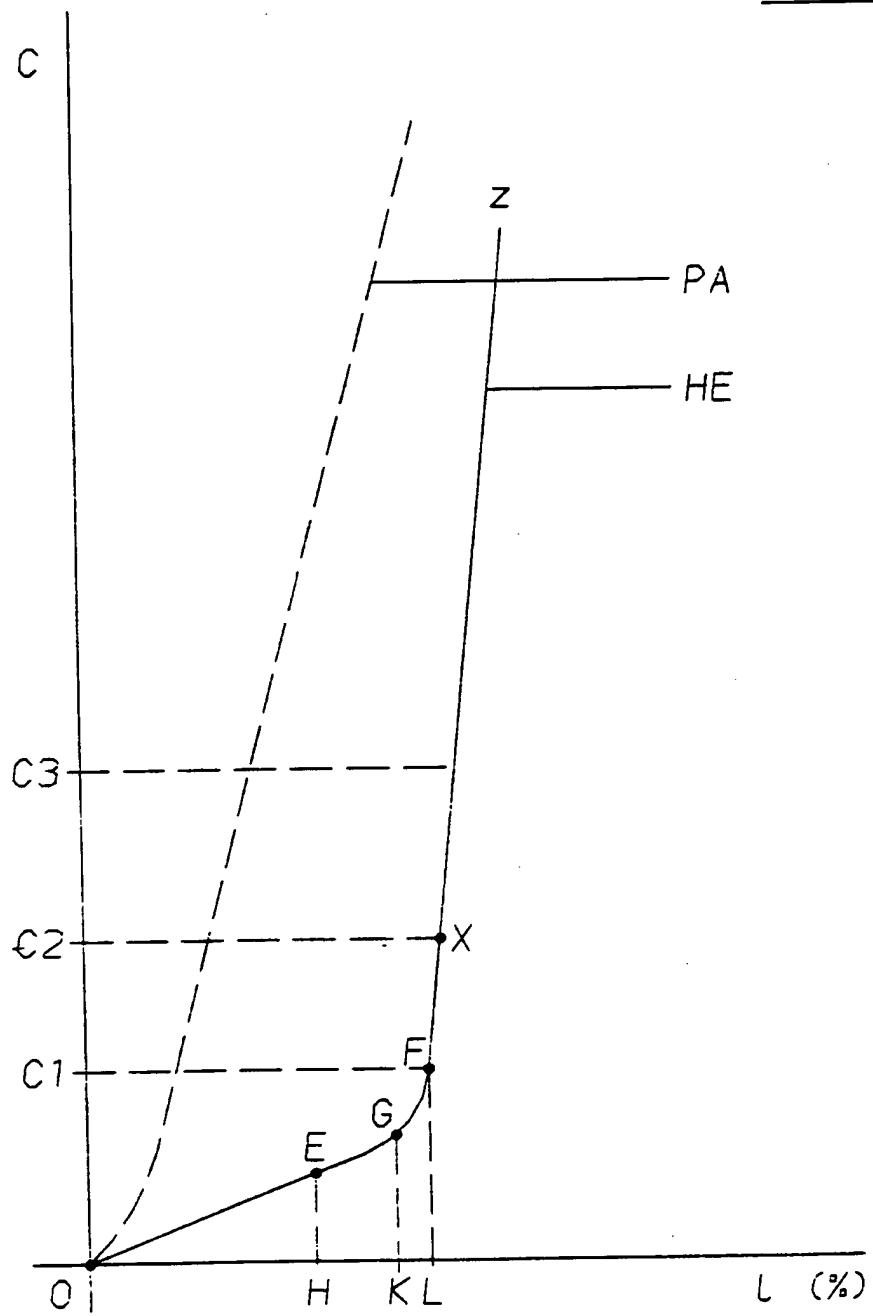


FIG 2



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FIG 3

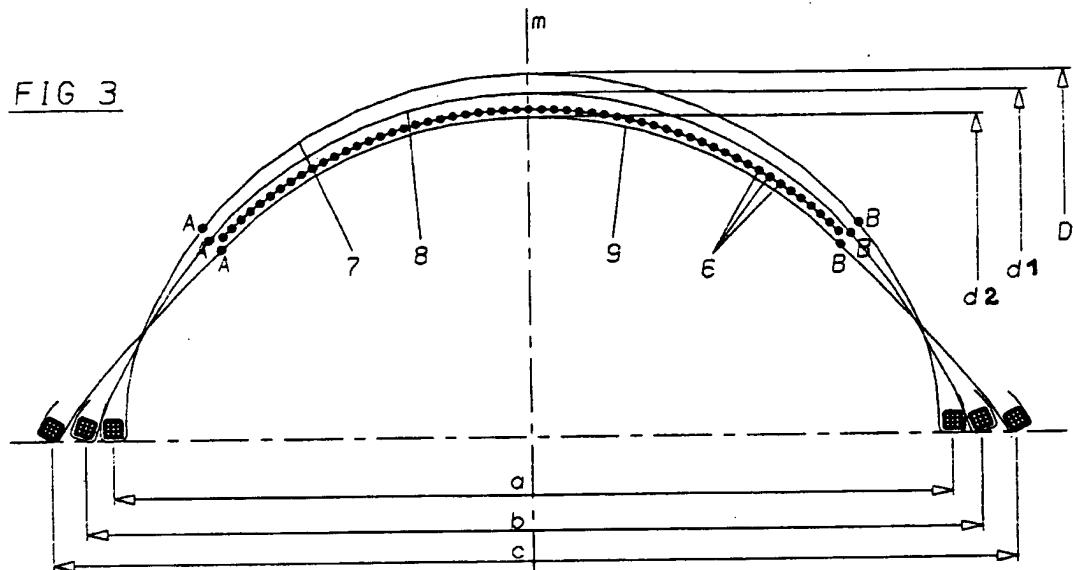
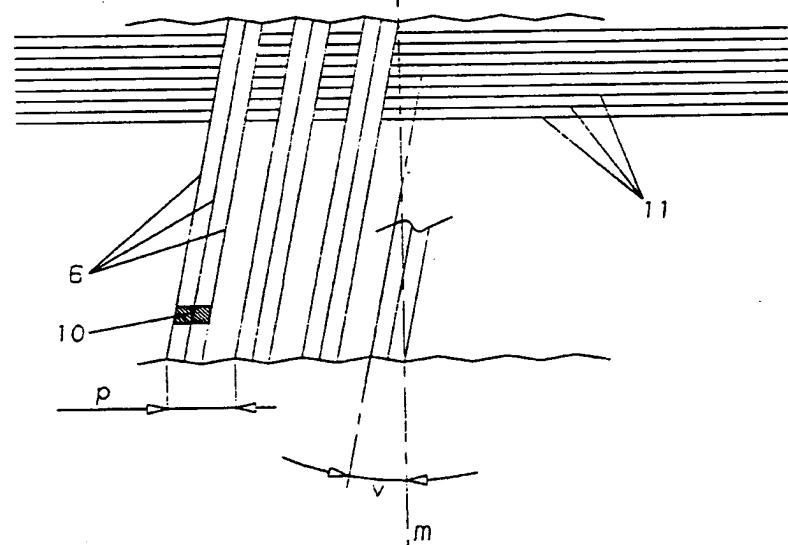


FIG 4



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